

to - CITY OF MIDDLETOWN LAND USE DEPARTMENTS

RINO MOZZICATO
PROPERTY AT
796 SAYBROOK ROAD
MIDDLETOWN, CT

.INCLUDING DRAINAGE
COMPUTATIONS SHOWING
NO IMPACT ON CITY
DRAINAGE FOR 25,50
OR 100 YEAR STORM

DEPT. PLANNING & ZONING
21 FEB 29 AM 10:19

from -
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2-28-2021



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DRAINAGE AREAS AND PATHWAYS

THE ENTIRE SITE DRAINS BY SHEET FLOW TO THE EXISTING STORM DRAINAGE IN SAYBROOK ROAD. THE 752 SAYBROOK ROAD SITE IS BEING DEVELOPED FOR A COMMERCIAL BUILDING AND ASSOCIATED PARKING.

THE LOT IS 54725 SF IN AREA. IT SLOPES FROM EAST TO WEST.

AS SHOWN ON THE "EXISTING DRAINAGE PLAN" THE DRAINAGE AREA IS 63000 SF AND STARTS IN THE EAST AS THE CENTER OF BARTHOMEW ROAD PAVING AND DRAINS WESTERLY TO THE EXISTING DRAINAGE IN SAYBROOK ROAD.

THE EXISTING SOILS ARE WETHERSFIELD WITH A LITTLE CHESHIRE ON THE NORTH END. THE EXISTING TIME OF CONCENTRATION IS 10 MINUTES. THE CHESHIRE SOILS GENERATE A 25 YEAR FLOW OF 0.42 CFS AND THE WETHERSFIELD SOILS 2.03 CFS FOR A TOTAL EXISTING FLOW OF 2.45 CFS. THE EXISTING DRAINAGE IN SAYBROOK ROAD HAS A PIPE RECEIVING STORM FLOW FROM THE SITE BETWEEN THE FORMER HOUSE AND ITS DRIVEWAY. THIS PIPE IS DAMAGED AND WILL BE REPLACED AS PART OF THE DEVELOPMENT AND ACT AS THE ONLY SITE OUTFALL.FROM THE DEVELOPED SITE.

METHODS TO REDUCE RATE OF RUNOFF

ANY DEVELOPMENT WILL INCREASE THE IMPERVIOUS AREAS DUE TO NEW BUILDINGS AND PARKING AREAS. THE INCREASE IN RATE OF RUNOFF AS WELL AS VOLUME OF RUNOFF WILL BE REDUCED BY HAVING THE RUNOFF DRAIN INTO LARGE UNDERGROUND STORAGE AREAS. THESE UNDERGROUND STORAGE AREAS WILL STORE THE WATER IN THE VOIDS AS WELL AS ENCOURAGE INFILTRATION INTO THE GROUND.

THE SOIL SURVEY SHOWS THE SITE HAS A DESIGN PERCOLATION OF 15 MINUTES TO THE INCH. THIS WAS CONFIRMED BY FIELD PERCOLATION TESTS. THIS PERCOLATION POTENTIAL ALLOWS FOR SIGNIFICANT INFILTRATION.

STORMWATER MANAGEMENT REFERENCE WORKS:

CONNECTICUT DOT DRAINAGE MANUAL

SCS -55

2004 SEDIMENT AND EROSION CONTROL MANUAL.

PLANS SHOWING
DRAINAGE

.
REFERENCE IS MADE
TO 24X36 INCH SHEETS
DR-EX S-2 D-1 D-2 D-3

.
REDUCED COPIES
OF THESE PLANS AT
END OF REPORT

.

DRAINAGE COMPUTATIONS FOR 796 SAYBROOK ROAD MIDDLETOWN CT
 TEMPLATE WITH THE AI METHOD USED

RATIONAL DRAINAGE COMPUTATIONS

RA_TEMPL

FOR

*

DRAINAGE DESIGN STORM IN YEARS

Years

DRAINAGE STRUCTURES I.D. NUMBERS OR DESCRIPTION

from structure

I.D. NUMBER #-

THRU PIPE I.D. #-

TO I.D. #-

FORMER DRIVEIN>SELF STORAGE

A - PAVED AREA

A - UNPAVED AREA

ACRES ADDED-

TOTAL ACRES TO PIPE-

PIPE MATERIAL

LENGTH FEET

PIPE SIZE in-

"n" VALUE

REF. SLOPE

CAP.DESIGN SLOPE

(to min. inlet HW)

FULL VELOCITY FPS

Q(f) CAPACITY CFS

DRAINAGE CHARACTERISTICS

T(C) MIN.-

TIME IN PIPE MIN.

TIME ACCUMULATED

RAIN - IN/HR-

I OR C PAVED

I OR C UNPAVED

AI OR AC-TO GRATE

AI OR AC- PAVED

AI OR AC- UNPAVED

SUM OF AI TO GRATE

SUM OF AI TO PIPE

Q TO SAYBROOK ROAD DRAINAGE CFS

Q THRU PIPE

EXISTING CONDITION

RA_AES

*

DRAINAGE DESIGN STORM IN YEARS

Years

DRAINAGE STRUCTURES I.D. NUMBERS OR DESCRIPTION

from structure

I.D. NUMBER #-

THRU PIPE I.D. #-

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FORMER DRIVEIN>SELF STORAGE

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PIPE MATERIAL

LENGTH FEET

PIPE SIZE in-

"n" VALUE

REF. SLOPE

CAP.DESIGN SLOPE

(to min. inlet HW)

FULL VELOCITY FPS

Q(f) CAPACITY CFS

DRAINAGE CHARACTERISTICS

T(C) MIN.-

TIME IN PIPE MIN.

TIME ACCUMULATED

RAIN - IN/HR-

I OR C PAVED

I OR C UNPAVED

AI OR AC-TO GRATE

AI OR AC- PAVED

AI OR AC- UNPAVED

SUM OF AI TO GRATE

SUM OF AI TO PIPE

Q TO SAYBROOK ROAD DRAINAGE CFS

Q THRU PIPE

EXISTING CONDITION

RA_AES

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DRAINAGE DESIGN STORM IN YEARS

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DRAINAGE STRUCTURES I.D. NUMBERS OR DESCRIPTION

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I.D. NUMBER #-

THRU PIPE I.D. #-

TO I.D. #-

FORMER DRIVEIN>SELF STORAGE

A - PAVED AREA

A - UNPAVED AREA

ACRES ADDED-

TOTAL ACRES TO PIPE-

PIPE MATERIAL

LENGTH FEET

PIPE SIZE in-

"n" VALUE

REF. SLOPE

CAP.DESIGN SLOPE

(to min. inlet HW)

FULL VELOCITY FPS

Q(f) CAPACITY CFS

DRAINAGE CHARACTERISTICS

T(C) MIN.-

TIME IN PIPE MIN.

TIME ACCUMULATED

RAIN - IN/HR-

I OR C PAVED

I OR C UNPAVED

AI OR AC-TO GRATE

AI OR AC- PAVED

AI OR AC- UNPAVED

SUM OF AI TO GRATE

SUM OF AI TO PIPE

Q TO SAYBROOK ROAD DRAINAGE CFS

Q THRU PIPE

EXISTING CONDITION

RA_AES

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DRAINAGE DESIGN STORM IN YEARS

Years

DRAINAGE STRUCTURES I.D. NUMBERS OR DESCRIPTION

from structure

I.D. NUMBER #-

THRU PIPE I.D. #-

TO I.D. #-

FORMER DRIVEIN>SELF STORAGE

A - PAVED AREA

A - UNPAVED AREA

ACRES ADDED-

TOTAL ACRES TO PIPE-

PIPE MATERIAL

LENGTH FEET

PIPE SIZE in-

"n" VALUE

REF. SLOPE

CAP.DESIGN SLOPE

(to min. inlet HW)

FULL VELOCITY FPS

Q(f) CAPACITY CFS

DRAINAGE CHARACTERISTICS

T(C) MIN.-

TIME IN PIPE MIN.

TIME ACCUMULATED

RAIN - IN/HR-

I OR C PAVED

I OR C UNPAVED

AI OR AC-TO GRATE

AI OR AC- PAVED

AI OR AC- UNPAVED

SUM OF AI TO GRATE

SUM OF AI TO PIPE

Q TO SAYBROOK ROAD DRAINAGE CFS

Q THRU PIPE

TEMPLET WITH THE AI METHOD USED

RATIONAL DRAINAGE COMPUTATIONS

RA_TEMPL
FOR

PROPOSED CONDITIONS

DRAINAGE DESIGN STORM IN YEARS
years

DRAINAGE STRUCTURES I.D. NUMBERS OR DESCRIPTION

from structure I.D. NUMBER #-
THRU PIPE I.D. #-
TO I.D. # -

ACRES - PAVED AREA
SF=
ACRES - UNPAVED AREA
SF=
ACRES ADDED-
TOTAL ACRES TOPIPE-

PIPE MATERIAL
LENGTH FEET
PIPE SIZE in-
"n" VALUE

REF. SLOPE
CAP.DESIGN SLOPE
(to min. inlet HW)
FULL VELOCITY FPS
Q(f) CAPACITY CFS

DRAINAGE CHARACTERISTICS

T(C) MIN.-
TIME IN PIPE MIN.
TIME ACCUMULATED
RAIN - IN/HR-
I OR C PAVED
I OR C UNPAVED
AI OR AC-TO GRATE
AI OR AC- PAVED
AI OR AC- UNPAVED

SUM OF AI TO GRATE
SUM OF AI TO PIPE

Q TO ON SITE DETENTION DRAINAGE CFS
Q THRU CB TO DETENTION

PROPOSED CONDITIONS

RA_AES

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25

ON SITE AREA P1
AREA P2
SOIL/BLD+PAVE
LOCATION
P2

0.05
2300.00
0.28
12150.00
0.33
0.33

FLOW TO SITE CB
FLOW
TO CB#16 IN P4

OVERLAND
NA
NA

10.00
NA
NA
5.60
0.90
0.25
0.05
0.07

0.12
0.12
CFS
0.66

*

25

ON SITE AREA P3
AREA P3
SOILS/PAVE
LOCATION
P3

0.24
10600.00
0.14
6150.00
0.38
0.38

FLOW TO SITE CB
FLOW
TO CB#14 IN P4

OVERLAND
NA
NA

10
NA
NA
5.60
0.90
0.25
0.22
0.04

0.25
0.37
CFS
1.42

*

25

ON SITE AREA P3
AREA P3
SOILS/PAVE
LOCATION
P4

0.25
10700.00
0.07
3000.00
0.31
0.31

FLOW TO SITE CB
FLOW
TO CB#16 IN P4

OVERLAND
NA
NA

10
NA
NA
5.60
0.90
0.25
0.22
0.02

0.24
0.24
CFS
1.33

*

25

ON SITE
AREAS P1+P2+P3+P4
SOILS/PAVE
LOCATION
TOTAL P1 P2 P3 P4

0.85
37050.00
0.56
24300.00
1.41
1.41

FLOW TO SITE CB
FLOW
TO DETENTION

OVERLAND
NA
NA

10
NA
NA
5.60
0.90
0.25
0.77
0.14

0.90
1.28
CFS
5.07
5.07

RAINFALL DATA

NOAA Atlas 14, Volume 10, Version 2
MIDDLETOWN 4 W
Station ID: 06-4767
Location name: Middletown, Connecticut, US*
Latitude: 41.5500°, Longitude: -72.7167°
Elevation:
Elevation (station metadata): 369 ft*
* source: Google Maps




POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wihite

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

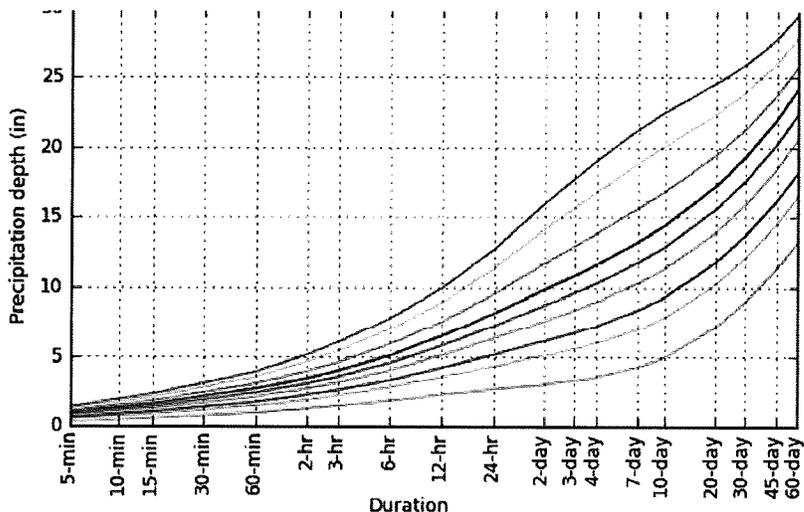
PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.328 (0.257-0.407)	0.401 (0.313-0.498)	0.520 (0.405-0.648)	0.618 (0.479-0.776)	0.754 (0.565-0.991)	0.859 (0.630-1.15)	0.964 (0.686-1.34)	1.09 (0.737-1.56)	1.26 (0.819-1.87)	1.39 (0.881-2.10)
10-min	0.464 (0.363-0.577)	0.568 (0.444-0.706)	0.736 (0.574-0.919)	0.876 (0.679-1.10)	1.07 (0.801-1.40)	1.22 (0.893-1.63)	1.37 (0.972-1.90)	1.55 (1.04-2.21)	1.79 (1.16-2.65)	1.97 (1.25-2.98)
15-min	0.546 (0.428-0.679)	0.668 (0.522-0.830)	0.866 (0.675-1.08)	1.03 (0.798-1.29)	1.26 (0.942-1.65)	1.43 (1.05-1.92)	1.61 (1.14-2.24)	1.82 (1.23-2.60)	2.10 (1.36-3.11)	2.32 (1.47-3.50)
30-min	0.751 (0.587-0.932)	0.912 (0.713-1.13)	1.18 (0.917-1.47)	1.40 (1.08-1.75)	1.70 (1.27-2.23)	1.93 (1.42-2.59)	2.16 (1.54-3.02)	2.45 (1.65-3.50)	2.83 (1.84-4.19)	3.12 (1.98-4.71)
60-min	0.955 (0.747-1.19)	1.16 (0.904-1.44)	1.49 (1.16-1.86)	1.76 (1.36-2.21)	2.14 (1.60-2.81)	2.43 (1.78-3.26)	2.72 (1.94-3.79)	3.08 (2.08-4.40)	3.56 (2.31-5.27)	3.92 (2.48-5.93)
2-hr	1.27 (0.999-1.56)	1.52 (1.20-1.87)	1.93 (1.52-2.39)	2.27 (1.78-2.83)	2.74 (2.08-3.58)	3.10 (2.30-4.16)	3.47 (2.50-4.84)	3.98 (2.69-5.64)	4.65 (3.02-6.84)	5.16 (3.28-7.74)
3-hr	1.47 (1.17-1.81)	1.76 (1.40-2.16)	2.23 (1.77-2.75)	2.63 (2.06-3.26)	3.16 (2.41-4.13)	3.58 (2.67-4.78)	4.00 (2.90-5.58)	4.61 (3.13-6.51)	5.41 (3.53-7.93)	6.03 (3.83-9.01)
6-hr	1.87 (1.50-2.27)	2.24 (1.79-2.73)	2.84 (2.27-3.48)	3.34 (2.65-4.12)	4.04 (3.10-5.23)	4.57 (3.44-6.07)	5.10 (3.74-7.08)	5.90 (4.03-8.29)	6.96 (4.55-10.1)	7.76 (4.95-11.5)
12-hr	2.29 (1.86-2.77)	2.77 (2.24-3.35)	3.56 (2.87-4.32)	4.21 (3.37-5.14)	5.11 (3.96-6.56)	5.80 (4.40-7.64)	6.49 (4.78-8.94)	7.51 (5.15-10.5)	8.86 (5.82-12.8)	9.88 (6.32-14.6)
24-hr	2.69 (2.20-3.22)	3.31 (2.71-3.97)	4.32 (3.52-5.20)	5.16 (4.17-6.25)	6.31 (4.94-8.07)	7.20 (5.51-9.45)	8.09 (6.02-11.1)	9.45 (6.51-13.1)	11.3 (7.41-16.2)	12.6 (8.10-18.5)
2-day	3.06 (2.53-3.63)	3.83 (3.16-4.56)	5.09 (4.19-6.08)	6.14 (5.01-7.38)	7.58 (5.99-9.66)	8.69 (6.73-11.4)	9.80 (7.39-13.5)	11.7 (8.05-16.0)	14.1 (9.32-20.1)	16.0 (10.3-23.2)
3-day	3.33 (2.77-3.94)	4.18 (3.48-4.96)	5.58 (4.62-6.64)	6.74 (5.54-8.07)	8.34 (6.63-10.6)	9.57 (7.45-12.5)	10.8 (8.19-14.8)	12.9 (8.94-17.7)	15.7 (10.4-22.3)	17.8 (11.5-25.8)
4-day	3.57 (2.99-4.22)	4.49 (3.75-5.30)	5.98 (4.97-7.09)	7.22 (5.96-8.61)	8.92 (7.12-11.3)	10.2 (7.99-13.3)	11.5 (8.78-15.8)	13.8 (9.58-18.9)	16.8 (11.1-23.8)	19.0 (12.3-27.5)
7-day	4.26 (3.59-4.99)	5.28 (4.44-6.19)	6.95 (5.82-8.18)	8.33 (6.93-9.88)	10.2 (8.22-12.9)	11.7 (9.19-15.1)	13.2 (10.0-17.9)	15.6 (10.9-21.2)	18.8 (12.5-26.5)	21.2 (13.7-30.5)
10-day	4.95 (4.19-5.77)	6.03 (5.10-7.04)	7.79 (6.57-9.14)	9.26 (7.74-10.9)	11.3 (9.08-14.1)	12.8 (10.1-16.4)	14.4 (10.9-19.3)	16.8 (11.8-22.8)	20.0 (13.4-28.2)	22.5 (14.6-32.2)
20-day	7.13 (6.10-8.25)	8.28 (7.08-9.60)	10.2 (8.66-11.8)	11.7 (9.92-13.7)	13.9 (11.2-17.1)	15.6 (12.3-19.6)	17.2 (13.0-22.6)	19.4 (13.7-26.0)	22.4 (15.0-31.1)	24.6 (16.0-35.0)
30-day	8.96 (7.72-10.3)	10.1 (8.73-11.7)	12.1 (10.4-14.0)	13.7 (11.6-16.0)	15.9 (12.9-19.4)	17.6 (13.9-21.9)	19.3 (14.6-25.0)	21.3 (15.1-28.4)	23.9 (16.1-33.2)	25.9 (16.9-36.8)
45-day	11.2 (9.74-12.9)	12.5 (10.8-14.3)	14.5 (12.5-16.7)	16.1 (13.8-18.7)	18.4 (15.0-22.2)	20.2 (16.0-24.8)	21.9 (16.5-27.9)	23.7 (16.9-31.4)	26.0 (17.6-35.8)	27.7 (18.1-39.2)
60-day	13.1 (11.4-15.0)	14.4 (12.5-16.4)	16.4 (14.2-18.9)	18.1 (15.6-21.0)	20.5 (16.8-24.6)	22.3 (17.7-27.3)	24.1 (18.2-30.5)	25.7 (18.4-33.9)	27.8 (18.9-38.2)	29.4 (19.2-41.4)

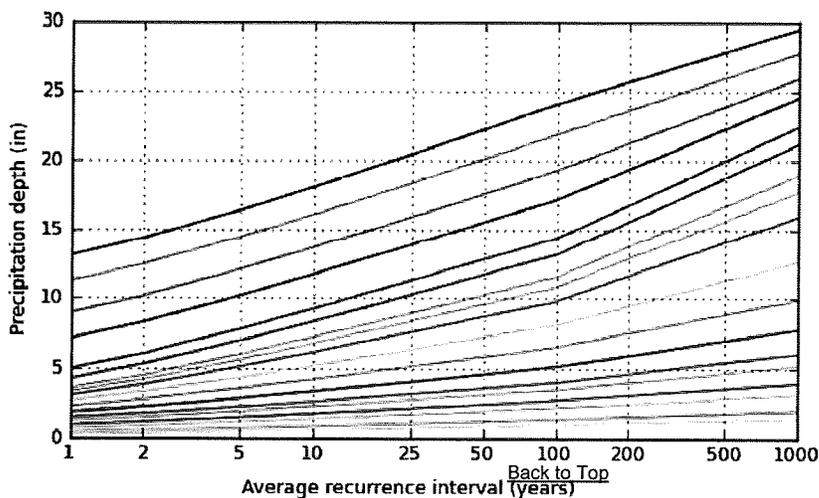
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000

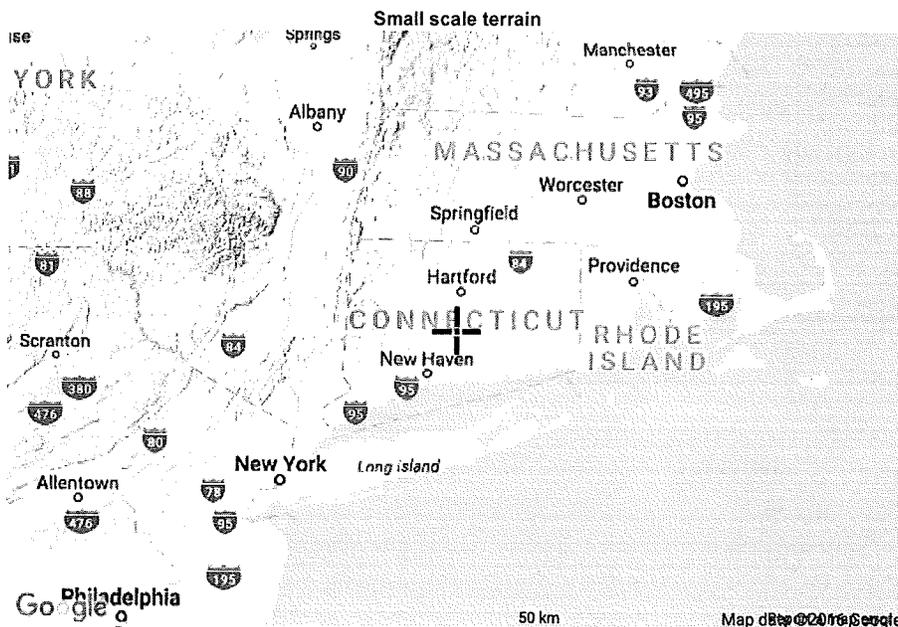


Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day

NOAA Atlas 14, Volume 10, Version 2

Maps & aeriels

Created (GMT): Mon Aug 15 12:09:11 2016



INFORMATION FROM
SCS SOIL SURVEY
ON SITE SOILS



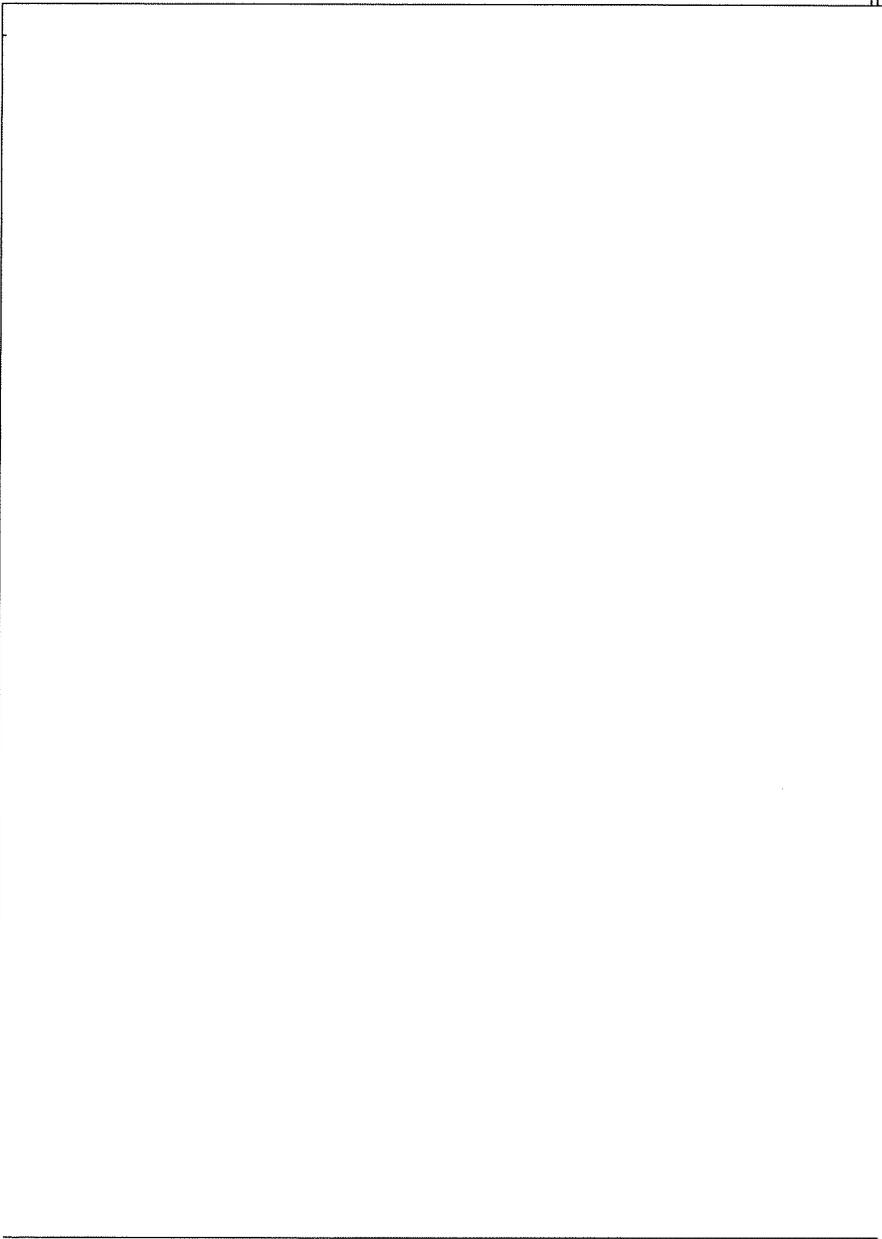
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Component Legend
Component Text Descriptions
Descripción de la Unidad de Mapa
Descripción de la Unidad de Mapa (Breve, Generada)
Legend
Map Unit Description
Options
Map Unit Description (Brief)
Map Unit Description (Brief, Generated)
Selected Soil Interpretation Description and Criteria Summary
Selected Soil Interpretations
Survey Area Data Summary
Survey Area Map Unit Symbols and Names
Water Quality Index (WQI) Soil Factors
Building Site Development
Construction Materials
Disaster Recovery Planning
Land Classifications
Land Management



Report — Map Unit Description

State of Connecticut
87B—Wethersfield loam, 3 to 8 percent slopes
Map Unit Setting
National map unit symbol: 9lrh
Elevation: 0 to 1,200 feet
Mean annual precipitation: 43 to 54 inches
Mean annual air temperature: 45 to 55 degrees F
Frost-free period: 140 to 185 days
Farmland classification: All areas are prime farmland

Map Unit Composition
Wethersfield and similar soils: 80 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wethersfield

**SEE DR-EX
FOR MAP
(4TH PAGE)**

Damage by Fire and Seedling Mortality on Forestland
Forestland Planting and Harvesting
Forestland Site Preparation
Haul Roads, Log Landings, and Soil Rutting on Forestland
Hazard of Erosion and Suitability for Roads on Forestland
Rangeland Fencing, Pygmy Rabbit Habitat, and Resistance to Fugitive Dust
Rangeland Invasive Species Susceptibility
Rangeland Mechanical Treatment by Chaining, Rolling Drum, and Shredder
Rangeland Site Degradation and Fire Damage Susceptibility
Rangeland Tillage, Compaction Resistance, and Soil Restoration
Recreational Development
Camp Areas, Picnic Areas, and Playgrounds
Paths, Trails, and Golf Fairways
Sanitary Facilities
Landfills
Sewage Disposal
Soil Chemical Properties
Chemical Soil Properties
Soil Erosion
Conservation Planning
RUSLE2 Related Attributes
Windbreaks and Environmental Plantings
Soil Health
Organic Matter Depletion, Salt Concentration, Aerobic Soil Organisms, Organic Soil Subsidence
Soil Health - Bulk Density and Texture
Soil Health - Compaction, Surface Sealing
Soil Health - Organic Matter
Soil Physical Properties
Engineering Properties
Fragments on the Soil Surface
Particle Size and Coarse Fragments
Physical Soil Properties
Soil Qualities and Features
Soil Features
Soil Locations
Vegetative Productivity
Environmental Plantings and Windbreaks
Forestland Productivity
Irrigated and Nonirrigated Yields by Map Unit Component
Irrigated Yields by Map Unit
Irrigated Yields by Map Unit Component
Link to Ecological Site Descriptions in EDIT
Nonirrigated Yields by Map Unit
Nonirrigated Yields by Map Unit Component
Rangeland and Forest Vegetation Classification, Productivity, and Plant Composition
Rangeland Productivity
Rangeland Productivity and Plant Composition
Waste Management
Agricultural Disposal of Manure, Food-Processing Waste, and Sewage Sludge
Agricultural Disposal of Wastewater by Irrigation and Overland Flow
Agricultural Disposal of Wastewater by Rapid Infiltration and Slow Rate Treatment
Large Animal Carcass Disposal

Setting

Landform: Drumlins, hills
Down-slope shape: Linear
Across-slope shape: Convex
Parent material: Coarse-loamy lodgment till derived from basalt and/or sandstone and shale

Typical profile

Ap - 0 to 3 inches: loam
Bw1 - 3 to 13 inches: loam
Bw2 - 13 to 27 inches: gravelly loam
Cd - 27 to 65 inches: gravelly loam

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: 20 to 40 inches to densic material
Drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 18 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 4.3 inches)

Interpretive groups

Land capability classification (Irrigated): None specified
Land capability classification (nonirrigated): 2e
Hydrologic Soil Group: C
Ecological site: F145XY012CT - Well Drained Dense Till Uplands
Hydric soil rating: No

Minor Components

Yalesville ←
Percent of map unit: 5 percent
Landform: Hills, ridges
Down-slope shape: Convex
Across-slope shape: Linear
Hydric soil rating: No

Ludlow

Percent of map unit: 5 percent
Landform: Drumlins, hills
Down-slope shape: Concave
Across-slope shape: Linear
Hydric soil rating: No

Cheshire

Percent of map unit: 5 percent
Landform: Hills, till plains
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

Wilbraham

Percent of map unit: 3 percent
Landform: Depressions, drainageways
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

Menlo

Percent of map unit: 2 percent
Landform: Depressions, drainageways
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

306—Udorthents—Urban land complex

Map Unit Setting

National map unit symbol: 9lmg
Elevation: 0 to 2,000 feet
Mean annual precipitation: 43 to 56 inches
Mean annual air temperature: 45 to 55 degrees F
Frost-free period: 120 to 185 days
Farmland classification: Not prime farmland

Map Unit Composition

Udorthents and similar soils: 50 percent
Urban land: 35 percent
Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents

Setting

Down-slope shape: Convex
Across-slope shape: Linear
Parent material: Drift

Typical profile

A - 0 to 5 inches: loam
C1 - 5 to 21 inches: gravelly loam

SOIL SURVEY

TABLE 14.--ENGINEERING PROPERTIES AND CLASSIFICATIONS--Continued

Soil name and map symbol	Depth in	USDA texture	Classification Unified	Classification AASHTO	Fragments > 3 inches	Percentage passing sieve number--				Liquidity limit	Plasticity index
						4	10	40	200		
W3 Walpole	0-10	Sandy loam	SN, OL	A-2, A-4	0-5	90-100	85-100	70-100	30-50	<25	NP-3 NP
	10-23	Fine sandy loam, sandy loam, gravelly sandy loam.	SN	A-2, A-4	0-5	85-100	60-100	40-95	25-50	---	
	23-60	Gravelly loamy sand, gravelly sand, sand.	SP, SM, GP	A-1, A-2, A-3	0-20	55-100	50-100	25-90	0-25	---	NP
W4 Westbrook	0-48	Mucky peat	Pt	A-8	0	---	---	---	---	---	NP
	48-93	Silt loam, very fine sandy loam, silt.	ML, CL-ML, OL	A-4	0	95-100	95-100	95-100	85-100	<25	NP-5
WkB, WkC, WkD Wethersfield	0-12	Loam	ML	A-4, A-5	0-5	85-95	80-95	65-85	55-70	<45	NP-8 NP-7
	12-26	Loam, silt loam, fine sandy loam.	ML	A-4, A-5	0-5	85-95	80-95	65-85	55-70	<45	
	26-60	Gravelly loam, loam, gravelly fine sandy loam.	SM, ML	A-4	0-10	75-90	70-90	55-80	40-65	<35	NP-7
WmB, WmC Wethersfield	0-12	Very stony loam	ML	A-4, A-5	10-20	85-95	80-95	65-85	55-70	<45	NP-8 NP-7
	12-26	Loam, silt loam, fine sandy loam.	ML	A-4, A-5	5-15	85-95	80-95	65-85	55-70	<45	
	26-60	Loam, gravelly loam, gravelly fine sandy loam.	SM, ML	A-4	0-10	75-90	70-90	55-80	40-65	<35	NP-7
WnC Wethersfield	0-12	Extremely stony loam.	ML	A-4, A-5	10-25	85-95	80-95	65-85	55-70	<45	NP-8
	12-26	Loam, silt loam, fine sandy loam.	ML	A-4, A-5	5-15	85-95	80-95	65-85	55-70	<45	
	26-60	Loam, gravelly loam, gravelly fine sandy loam.	SM, ML	A-4	0-10	75-90	70-90	55-80	40-65	<35	
Wf Wilbraham	0-4	Silt loam	ML	A-4, A-5	0-5	80-95	70-95	65-85	55-70	<45	
	4-20	Loam, silt loam, loam.	ML	A-4, A-5	0-5	80-95	70-95	65-85	55-70	<45	

DRAINAGE CALCULATION NARRATIVE

WE HAVE BASED OUR REPORT ON THE 25 YEAR STORM AS REQUIRED BY THE DOT.
WE HAVE INCLUDED SUPPLEMENTAL DRAINAGE CALCULATIONS FOR 50 AND 100 YEAR STORMS .

PURPOSE OF 25 YEAR DRAINAGE CALCULATION IS TO SHOW THAT THE DEVELOPMENT WILL NOT HAVE AN ADVERSE IMPACT ON THE TOWN ROAD.

THE EXISTING SITE WATERSHED IS DEPICTED ON THE PREVIOUS GRAPHIC.
THE TOTAL DRAINAGE AREA DEVELOPED IS 63000+ S.F.
OF THIS TOTAL 31659 SF (37050SF 4275 1030 86 EX EX. IMP) WILL BE CONVERTED TO IMPERVIOUS SURFACES.

BECAUSE OF THE SMALL WATERSHED, WE PROPOSE TO USE VOLUME CALCULATIONS OF TOTAL RUNOFF FOR A ONE HOUR STORM.

AS CALCULATED ON THE FOLLOWING SHEETS FOR THE 31659 SF OF NEW IMPERVIOUS AREA:
COEFFECIENT OF RUNOFF C EXISTING C=.3 VOLUME (25) EXISTING =3647 CF
COEFFECIENT OF RUNOFF C PROPOSED C=.63 VOLUME (25)PROPOSED=7634 CF
INCREASE IN VOLUME OF RUNOFF =3986 CF
Q(25) EXIST = .42+2.03=2.45 CFS Q PROP= 5.07 CFS INCREASE CREATED = 2.62 CFS
BOTH BASED ON A 10 MINUTE TIME OF CONCENTRATION.

ON SITE DETENTION

TO MINIMIZE THE RATE OF RUNOFF FROM THE DEVELOPMENT, ON SITE DETENTION WAS CREATED FOR THE VOLUME OF INCREASE IN RUNOFF FOR THE 25, 50 AND 100 YEAR STORM.

FROM THE 31659 SF MADE IMPERVIOUS;

NEW VOLUME V(new) =3986 CF

STORAGE PROVIDED = 5685 CF STATIC STORAGE AND 7845 CF TOTAL STORAGE.

ON SITE OUTFALL

OUTFALL FROM THE DETENTION AREA IS RESTRICTED BY A 4" ORIFICE. COMPUTED MAXIMUM FLOW THRU THE ORIFICE IS LESS THAN 1.0 CFS.

rational computation flow = AREA P1 P2 P3 P4 MAXIMUM FLOW =1.65 cfs FOR P2 (P1=.66/P2=1.65/P3=1.42/P4=1.33)

CHECK CAPACITY OF PIPES 15" PVC S=.01 n=.013

Q(full) capacity = 6.73 cfs >> 1.65 cfs

v(full) = 5.48 fps > 10 fps suggested limit.

ok

Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 25- year storm

796 SAYBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

During a 25 year storm approximately 2.3 inches of rain will fall in one hour.
 Underexisting conditions, almost 10% to 30% of this rainfall would normally be runoff. 90% will be runoff from the new impervious areas.

$I = 2.3 \text{ in/hr}$ or 0.192 ft/hr for a 25- year storm

Existing Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Total:	63000			
Grass:	57074	1.31	0.24 (use average of C)	
Impervious former house/drive/ROAD:	5926	0.14	0.9	
Total:	63000	1.45		
Weighted 'C':	0.30			
EX.VOLUME RUNOFF=	0.30	63000	0.192 =	3647.639 CF ←

Proposed Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Grass:	25950	0.60	0.25	
Existing Impervious:	4896	0.11	0.9	
Proposed Impervious:	32154	0.74	0.9	
Total:	63000	1.45		
Weighted 'C':	0.63			
EX.VOLUME RUNOFF=	0.63	63000	0.192 =	7634.563 CF ←
				3986.924 ←

$Q = c I A$



Drainage Calculations
RINO MOZZICATO
COMMERCIAL
796 SA YBROOK ROAD MIDDLETOWN CT

for a 25- year storm

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED
Volume of New Runoff

Volume of TOTAL Runoff

for a 25- year storm

$$V_{new} = (C_{prop} - C_{ex}) * I * A$$

$$V_{total} = C_{prop} * I * A$$

C_{prop}	0.63	C_{prop}	0.63
C_{ex}	0.30		
I	1.000 in/hr	I	1.000 in/hr
A	1.45 Ac.	A	1.45 Ac.
Q=	0.478 CFS		0.914 CFS
Vnew=	1719 CF	Vtotal=	3292 CF
	for the first inch rainfall		for the first inch rainfall

$$V_{new} = (C_{prop} - C_{ex}) * I * A$$

$$V_{total} = C_{prop} * I * A$$

C_{prop}	0.63	C_{prop}	0.63
C_{ex}	0.30		
I	2.300 in/hr	I	2.300 in/hr
A	1.45 Ac.	A	1.45 Ac.
Q=	1.098 CFS		2.103 CFS
Vnew=	3954 CF (HOUR)	Vtotal=	7635 CF (HOUR)
	for a 25- year storm		for a 25- year storm

Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 25- year storm

796 SAYBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

Volume of Storage- Pipes USED= YES

Pipe:

Dia. 30 inches
Stores: 4.91 cf/ ft length

Stone:

Trench Width: 6 ft
Trench Depth: 6 ft
Void Ratio: 0.35
Stores: 10.88 cf/ ft length

Total Storage:

4.91 + 10.88 = 15.79 cf/ ft length

Infiltration

DESIGN INFILTRATION RATE 15 MIN/INCH

Infiltration Rate= DESIGN 15.00 min/in or 4.00 in/hr
or 0.33 ft/hr

Surface Area Trench=2sides+bottom= 18 sf/ ft length

0.33 ft/hr * 18.00 sf/ ft length = 6.00 cf/hr/ ft length

Total Absorption= 15.79 cf/ ft length + 6.00 cf/hr/ ft length= 21.79 cf/ ft length

Therefore,

Storage Required:			3954 cf		
STORAGE PROVIDED				% OF REQ.	
0.0112 Storage Provided- Drywells:	0 drywells *	724 cf storage/ drywell=	0 cf		
89.3167 Storage Provided- Pipe:	360 ft *	15.79 cf storage/ ft length=	5685 cf	=>req.first inch runoff=	3292 cf
INFILTRATION Provided- Pipe:	360 ft *	6.00 cf storage/ ft length=	2160 cf		
		Total:	7845 cf	198% of new runoff=	3954 cf

Storage provided exceeds storage required
discharge rate to EX. ROAD DRAINAGE limited by 4" outfall orifice



Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 50- year storm

796 SAYBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

During a 50 year storm approximately 2.43 inches of rain will fall in one hour.
 Under existing conditions, almost 10% to 30% of this rainfall would normally be runoff. 90% will be runoff
 from the new impervious areas.

I= 2.43 in/hr or 0.203 ft/hr for a 50- year storm

Existing Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Total:	63000			
Grass:	57074	1.31	0.24 (use average of C)	
Impervious former house/drive/ROAD:	5926	0.14	0.9	
Total:	63000	1.45		
Weighted 'C':	0.30			
EX.VOLUME RUNOFF=	0.30	63000	0.203 =	3853.81 CF

Proposed Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Grass:	25950	0.60	0.25	
Existing Impervious:	4896	0.11	0.9	
Proposed Impervious:	32154	0.74	0.9	
Total:	63000	1.45		
Weighted 'C':	0.63			
EX.VOLUME RUNOFF=	0.63	63000	0.203 =	8066.081 CF
			INCREASE	4212.271 CF

$Q = c I A$



Drainage Calculations
RINO MOZZICATO
COMMERCIAL

796 SA YBROOK ROAD MIDDLETOWN CT

for a 50- year storm

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

Volume of New Runoff

Volume of TOTAL Runoff

$V_{new} = (C_{prop} - C_{ex}) * I * A$

$V_{total} = C_{prop} * I * A$

C_{prop} 0.63
 C_{ex} 0.30
 I 1.000 in/hr
 A 1.45 Ac.
 $Q =$ 0.478 CFS
 $V_{new} =$ 1719 CF

C_{prop} 0.63
 I 1.000 in/hr
 A 1.45 Ac.
 $Q =$ 0.914 CFS
 $V_{total} =$ 3292 CF

for the first inch rainfall for the first inch rainfall

for a 50- year storm

$V_{new} = (C_{prop} - C_{ex}) * I * A$

$V_{total} = C_{prop} * I * A$

C_{prop} 0.63
 C_{ex} 0.30
 I 2.430 in/hr
 A 1.45 Ac.
 $Q =$ 1.160 CFS
 $V_{new} =$ 4177 CF (HOUR)

for a 50- year storm

C_{prop} 0.63
 I 2.430 in/hr
 A 1.45 Ac.
 $Q =$ 2.222 CFS
 $V_{total} =$ 8066 CF (HOUR)

for a 50- year storm

Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 50- year storm

796 SA YBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

Volume of Storage- Pipes USED= YES

Pipe:

Dia. 30 inches
 Stores: 4.91 cf/ ft length

Stone:

Trench Width: 6 ft
 Trench Depth: 6 ft
 Void Ratio: 0.35
 Stores: 10.88 cf/ ft length

Total Storage:

4.91 + 10.88 = 15.79 cf/ ft length

Infiltration

DESIGN INFILTRATION RATE 15 MIN/INCH

Infiltration Rate= DESIGN 15.00 min/in or 4.00 in/hr
 or 0.33 ft/hr

Surface Area Trench=2sides+bottom= 18 sf/ ft length

0.33 ft/hr * 18.00 sf/ ft length = 6.00 cf/hr/ ft length

Total Absorption= 15.79 cf/ ft length + 6.00 cf/hr/ ft length= 21.79 cf/ ft length

Therefore,

Storage Required:			4177 cf		
STORAGE PROVIDED				% OF REQ.	
0.0112 Storage Provided- Drywells:	0 drywells *	724 cf storage/ drywell=	0 cf		
89.3167 Storage Provided- Pipe:	360 ft *	15.79 cf storage/ ft length=	5685 cf	=>req.first inch runoff=	3292 cf
INFILTRATION Provided- Pipe:	360 ft *	6.00 cf storage/ ft length=	2160 cf		
		Total:	7845 cf	188% of new runoff=	4177 cf

Storage provided exceeds storage required
 discharge rate to EX. ROAD DRAINAGE limited by 4" outfall orifice



Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 100- year storm

796 SAYBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

During a 100 year storm approximately 3 inches of rain will fall in one hour.
 Underexisting conditions, almost 10% to 30% of this rainfall would normally be runoff. 90% will be runoff
 from the new impervious areas.

I= 3 in/hr or 0.250 ft/hr for a 100- year storm

Existing Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Total:	63000			
Grass:	57074	1.31	0.24 (use average of C)	
Impervious former house/drive/ROAD:	5926	0.14	0.9	
Total:	63000	1.45		
Weighted 'C':	0.30			
EX.VOLUME RUNOFF=	0.30	63000	0.250 =	4757.79 CF

Proposed Conditions: OF AREA DEVELOPED

	Area (sf)	Area (Ac.)	C	
Grass:	25950	0.60	0.25	
Existing Impervious:	4896	0.11	0.9	
Proposed Impervious:	32154	0.74	0.9	
Total:	63000	1.45		
Weighted 'C':	0.63			
EX.VOLUME RUNOFF=	0.63	63000	0.250 =	9958.125 CF
				5200.335

$Q = c I A$



Drainage Calculations
RINO MOZZICATO
COMMERCIAL

796 SAYBROOK ROAD MIDDLETOWN CT

for a 100- year storm

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

Volume of New Runoff

Volume of TOTAL Runoff

for a 100- year storm

$V_{new} = (C_{prop} - C_{ex}) * I * A$

$V_{total} = C_{prop} * I * A$

C_{prop} 0.63
 C_{ex} 0.30
 I 1.000 in/hr
 A 1.45 Ac.
 $Q =$ 0.478 CFS
 $V_{new} =$ 1719 CF
 for the first inch rainfall

C_{prop} 0.63
 I 1.000 in/hr
 A 1.45 Ac.
 $Q =$ 0.914 CFS
 $V_{total} =$ 3292 CF
 for the first inch rainfall

$V_{new} = (C_{prop} - C_{ex}) * I * A$

$V_{total} = C_{prop} * I * A$

C_{prop} 0.63
 C_{ex} 0.30
 I 3.000 in/hr
 A 1.45 Ac.
 $Q =$ 1.433 CFS
 $V_{new} =$ 5157 CF (HOUR)
 for a 100- year storm

C_{prop} 0.63
 I 3.000 in/hr
 A 1.45 Ac.
 $Q =$ 2.743 CFS
 $V_{total} =$ 9958 CF (HOUR)
 for a 100- year storm



Drainage Calculations
RINO MOZZICATO
COMMERCIAL

for a 100- year storm

796 SAYBROOK ROAD MIDDLETOWN CT

796 SAY 221103 Infiltration(Pkhr).xlsx

Drainage Area ENTIRE AREA DEVELOPED

Volume of Storage- Pipes USED= YES

Pipe:

Dia. 30 inches
 Stores: 4.91 cf/ ft length

Stone:

Trench Width: 6 ft
 Trench Depth: 6 ft
 Void Ratio: 0.35
 Stores: 10.88 cf/ ft length

Total Storage:

4.91 + 10.88 = 15.79 cf/ ft length

Infiltration

DESIGN INFILTRATION RATE 15 MIN/INCH

Infiltration Rate= DESIGN 15.00 min/in or 4.00 in/hr
 or 0.33 ft/hr

Surface Area Trench=2sides+bottom= 18 sf/ ft length

0.33 ft/hr * 18.00 sf/ ft length = 6.00 cf/hr/ ft length

Total Absorption= 15.79 cf/ ft length + 6.00 cf/hr/ ft length= 21.79 cf/ ft length

Therefore,

Storage Required:			5157 cf		
STORAGE PROVIDED				% OF REQ.	
0.0112 Storage Provided- Drywells:	0 drywells *	724 cf storage/ drywell=	0 cf		
89.3167 Storage Provided- Pipe:	360 ft *	15.79 cf storage/ ft length=	5685 cf	=>req.first inch runoff=	3292 cf
INFILTRATION Provided- Pipe:	360 ft *	6.00 cf storage/ ft length=	2160 cf		
		Total:	7845 cf	152% of new runoff=	5157 cf

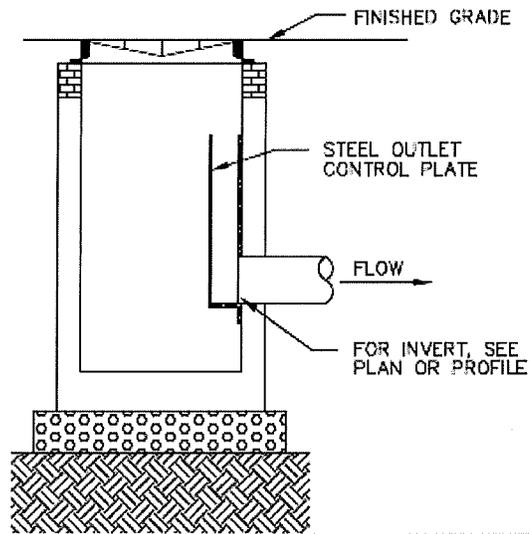
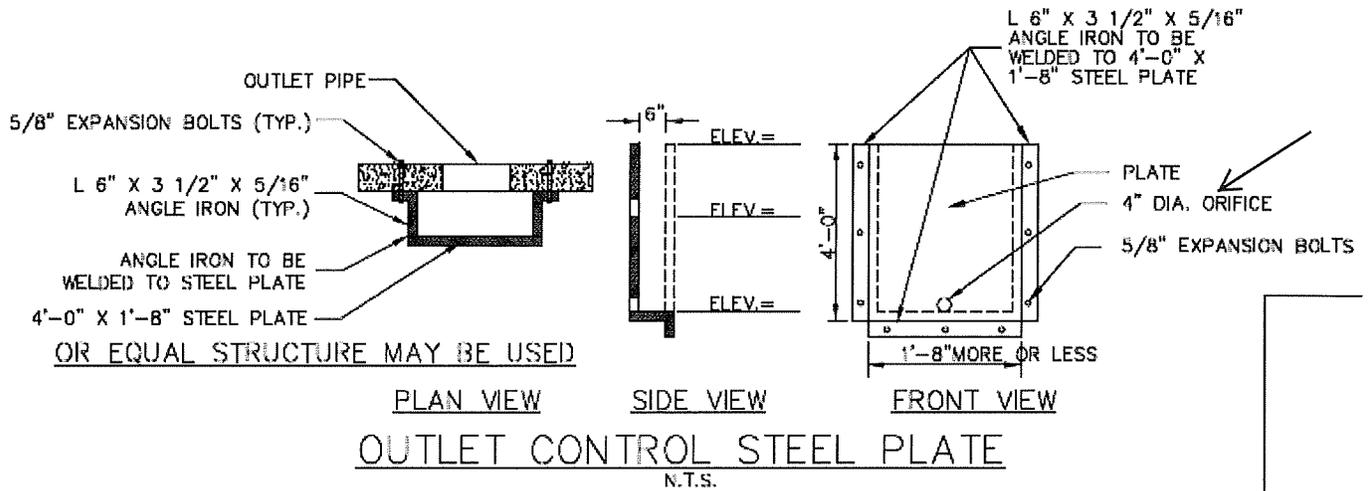
Storage provided exceeds storage required
 discharge rate to EX. ROAD DRAINAGE limited by 4" outfall orifice



ORIFICE DATA

RESTRICTS FLOW
TO PREVENT INCREASE
RATE OF RUNOFF TO
WATERCOURSE BEFORE
DOT BOX CULVERT.

OUTLET CONTROL FROM STORM MH #34 LIMITED BY 4 INCH ORIFICE WHICH DRAINS INTO 8" PIPE OUTFALL #47 (LARGER TO PREVENT CLOGGING BY RODENTS)

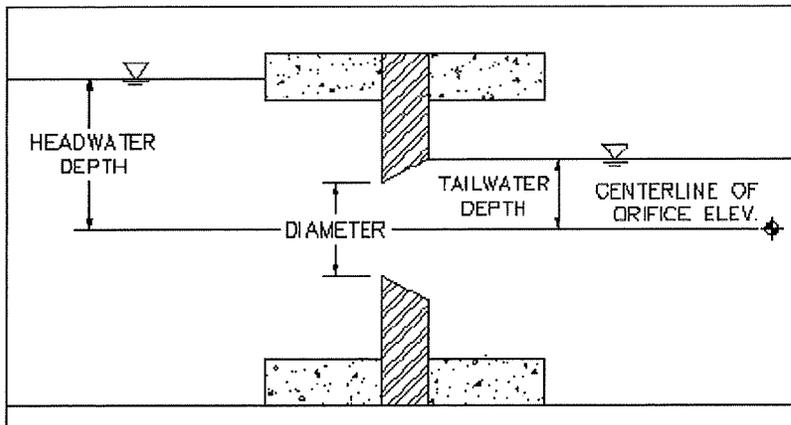


Screen clipping taken: 8/16/2016 9:22 AM

DETAIL FROM SHEET D-2

Use the Orifice Calculator to calculate hydraulic values for orifices.

The following illustration shows orifice values:



Orifice values

The structure height, headwater, and tailwater are all measured from the center of the orifice.

The Orifice Calculator uses the following formula:

$$Q = cA\sqrt{2gH}$$

where:

- Q = Design flow rate
- c = Orifice coefficient
- A = Cross-sectional area
- g = Acceleration due to gravity (32.174 ft/s² or 9.807 m/s²)
- H = Total head (Headwater minus Tailwater)

Screen clipping taken: 8/16/2016 10:32 AM

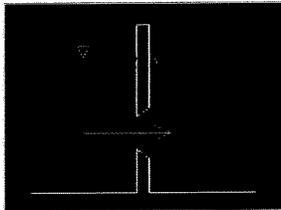
sharp-edged orifices have coefficients around 0.6 to 0.63

Screen clipping taken: 8/16/2016 9:23 AM

Orifice Calculator [X]

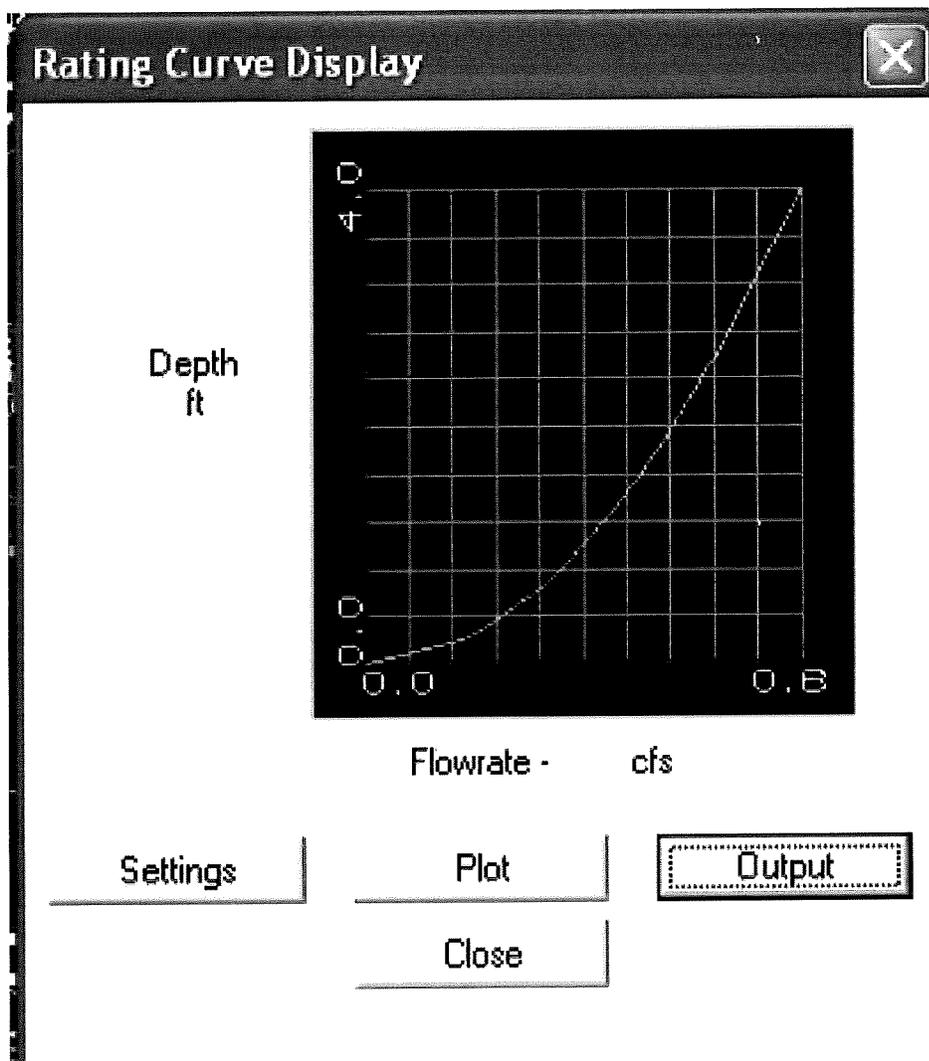
Solve For: Use: Diameter Area

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Diameter	in	<input type="text" value="4.0000"/>	Select
Area	ft ²	<input type="text" value="0.0000"/>	Select
Headwater	ft	<input type="text" value="4.0000"/>	
Tailwater	ft	<input type="text" value="0.0000"/>	
Velocity	fps	9.6261	



Rating | Output | **OK** | Cancel | Help

Screen clipping taken: 8/16/2016 10:26 AM



Screen clipping taken: 8/16/2016 10:24 AM

#Units=Structural Dimensions,in,Flowrate,cfs

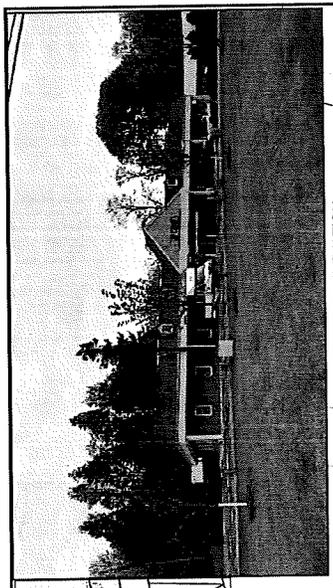
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#Depth - ft Flowrate - cfs

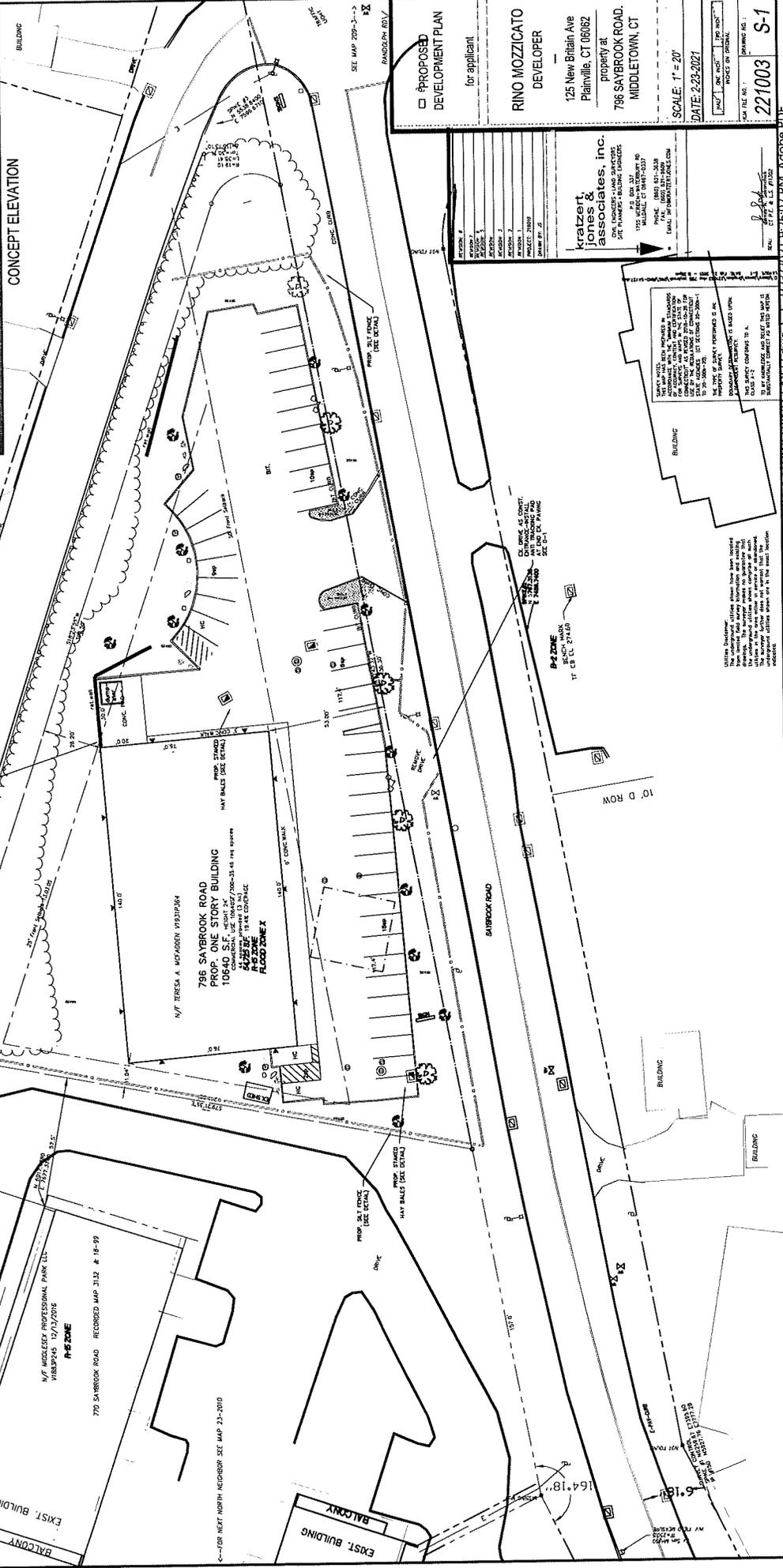
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REDUCED SITE PLANS



CONCEPT ELEVATION



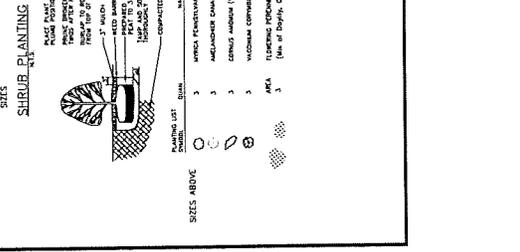
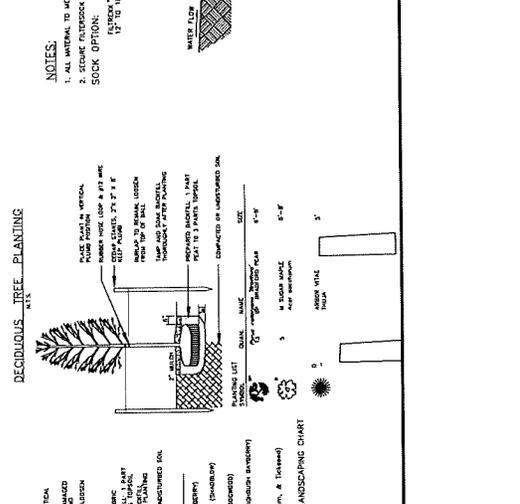
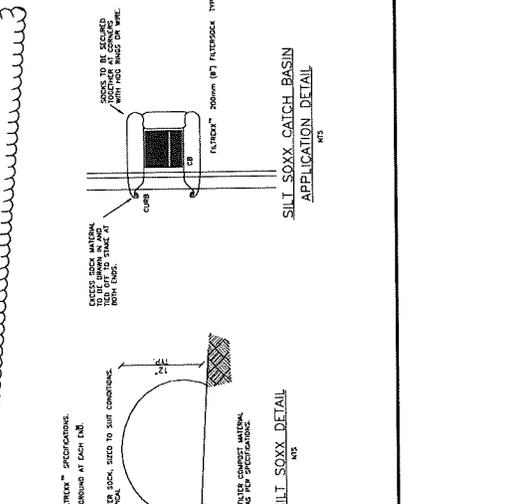
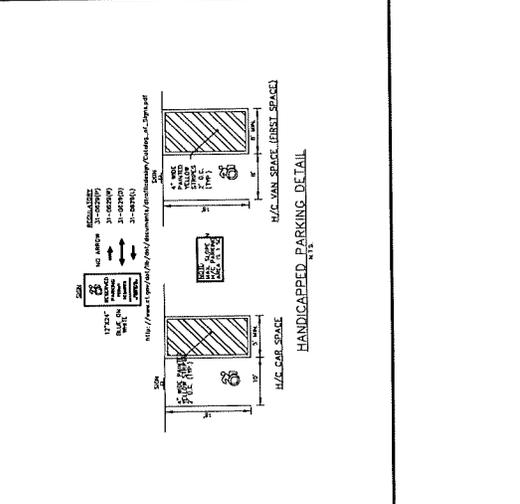
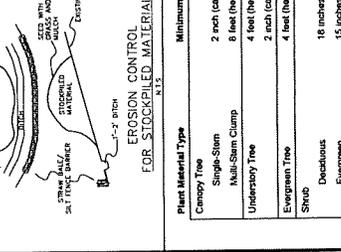
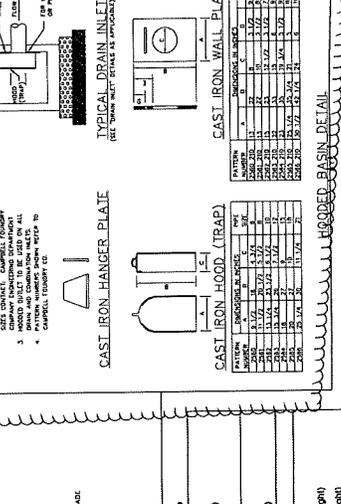
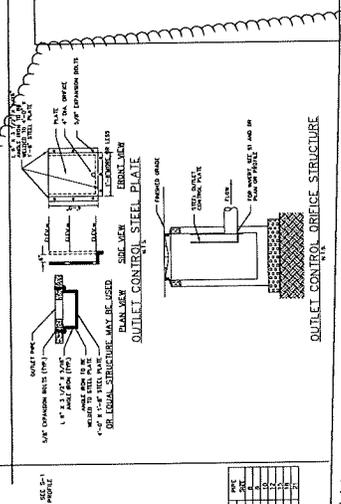
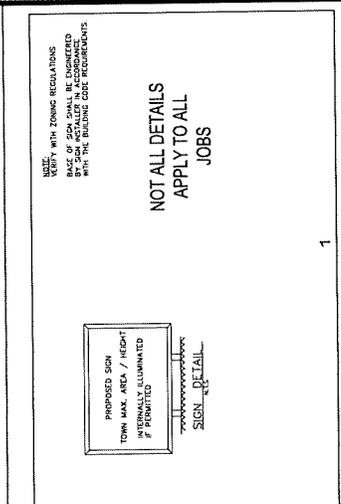
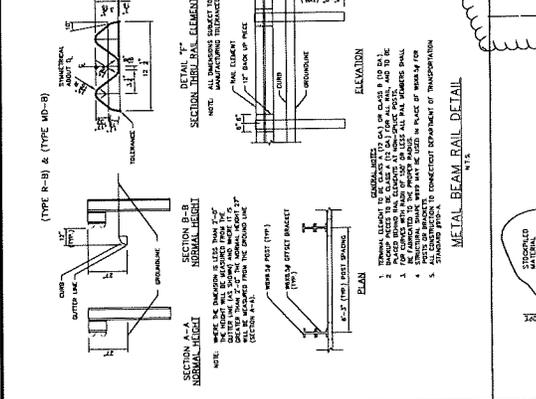
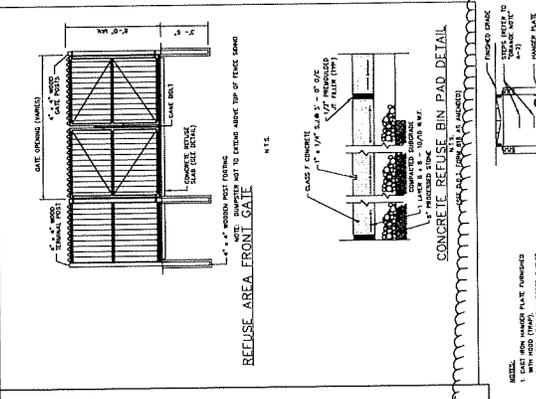
BUILDING LIGHTS MOUNTED AT 24 FT

Lighting Schedule

Item	Description	Quantity	Notes
1	LED Wall Light	10	24 ft height
2	LED Downlight	5	5 ft height
3	LED Track Light	15	24 ft height
4	LED Recessed Light	10	5 ft height
5	LED Flood Light	5	24 ft height

D-Series Slim 1 LED Wall Luminaires

Model	Height	Width	Depth	Weight	Notes
D-1	24"	12"	4"	1.5 lbs	Standard
D-2	24"	18"	4"	2.5 lbs	Standard
D-3	24"	24"	4"	3.5 lbs	Standard
D-4	24"	30"	4"	4.5 lbs	Standard
D-5	24"	36"	4"	5.5 lbs	Standard



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